Appl. No. 10/656,257 Amendment Dated October 12, 2004

Response to Office Action of April 13, 2004

REMARKS/ARGUMENT

This letter is responsive to the Office Action mailed on April 13, 2004. The claims have

been amended in response to the outstanding Office Action. No new matter has been

added by the amendments.

Claims 1 to 7, as amended, are currently pending in the application.

Claims 1 to 5 and 7 are rejected under 35 U.S.C. §102(b) in view of Fisher

The Examiner has rejected claims 1 to 5 and 7 under 35 U.S.C. §102(b) as being

anticipated by Fisher (U.S. Patent No. 6,040,752).

Specifically, the Examiner states that the Fisher reference discloses a linear switch

actuator (Fisher, FIGS. 4 and 6) for actuating a moveable element having a soft iron

yoke (44), a magnetic coil (43) positioned within the yoke (44), and a moveable

armature assembly (40, 41, 42) adapted to be coupled to the movable element. The

moveable armature assembly includes a soft-iron armature (40) having permanent

magnets (41 and 42) at its ends with opposite pole orientations and being movable

between a first stroke end position (Fisher, FIG. 4) and a second stroke end position

(Fisher, FIG. 6).

In response, the Applicants have amended claims 1 to 7 to better clarify the distinction

between the present invention as claimed and the cited prior art references.

Independent claim 1, as amended, defines a linear switch actuator having a

ferromagnetic shield having a hollow tubular portion and first and second end plates,

where first and second apertures are formed within said first and second end plates,

and where the shield defines a single and uninterrupted internal region that extends

between the inside surfaces of the hollow tubular portion. A magnetic coil (16) is

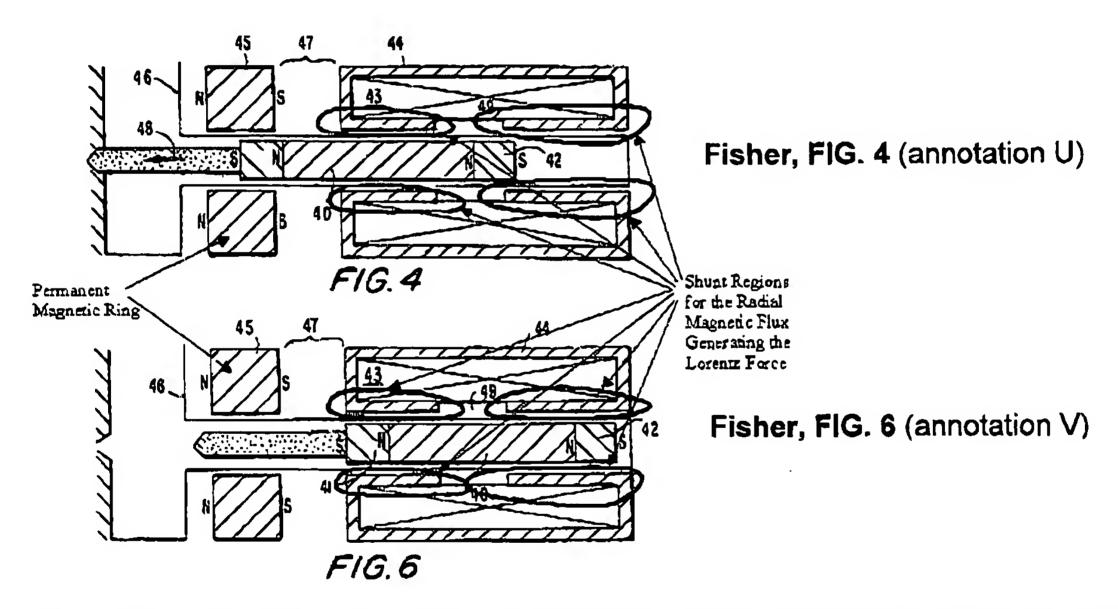
-5-

BEST AVAILABLE COPY

Appl. No. 10/656,257 Amendment Dated October 12, 2004 Response to Office Action of April 13, 2004

positioned within the interior region. A moveable armature assembly (12, 14a, 14b) having two permanent magnets (14a, 14b) at the ends is positioned along the longitudinal axis of the coil (16) and extends through the first and second apertures of the shield (18). Support for these amendments are provided in the subject disclosure (Disclosure, page 9, line 3 to page 13, line 20 and FIGS. 4, 5A, 5B, 6, 7A, 7B, and 7C).

The electromagnetic actuator (Fisher, abstract) of Fisher uses a solenoid (43) positioned within a yoke (44) having shunt regions (as shown in Fisher, FIG. 4 (annotation U) and Fisher, FIG. 6 (annotation V) below) as well as a permanent magnet ring (45) to move an actuator (40, 41, 42) between two positions.



Fisher's ferromagnetic yoke (44) includes shunt regions (as circled above in Fisher, FIG. 4 (annotation U) and Fisher, FIG. 6 (annotation V)) on either side of the gap (49). These shunt regions are necessary for the proper operation of Fisher, as will be described.

In conventional electromagnetic actuators like the one disclosed in Fisher, active forces are generated by the air-gap magnetic flux of the electro-magnet. This phenomenon is discussed in Fisher and in the subject disclosure, (Disclosure, page 2, lines 11 to page

Appl. No. 10/656,257 Amendment Dated October 12, 2004 Response to Office Action of April 13, 2004

3, line 3, and FIG. 1). Within the electromagnetic actuator of Fisher, the radial magnetic flux is detrimental to the operation of the actuator. The circled shunt portions of the yoke (44) (shown above) shunt the radial magnetic field that would otherwise flow from the armature assembly through the coil and to the outer wall of the yoke (44). The shunt regions serve to collect magnetic flux, otherwise traversing radially across the solenoid (43), and introduce it directly into the yoke (44) through the axial ends of the yoke (44). By means of the shunt regions, the yoke (44) presents discrete pole surfaces to the moving armature (40, 41, 42) such that the magnetic influences of both the yoke (44) alone (unpowered) and the yoke (44) and solenoid (43) combination (powered) are defined in terms of the magnetic state of the ends of the yoke (44).

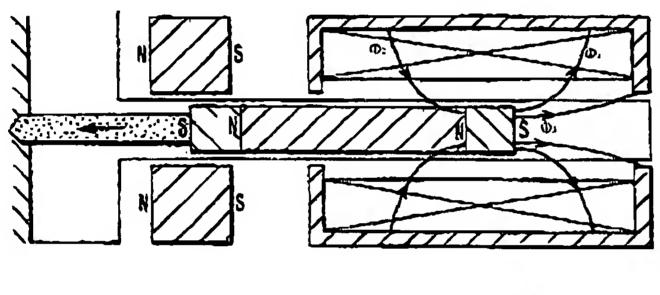


FIG. X: Magnetic flux path in Fisher actuator where the shunt regions of yoke (44) are <u>hypothetically</u> removed

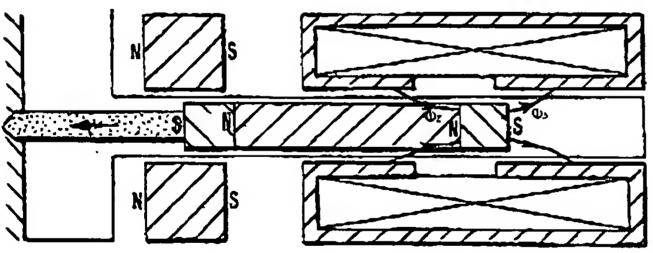


FIG. Y: Magnetic flux path in Fisher actuator showing yoke (44) having disclosed shunt regions

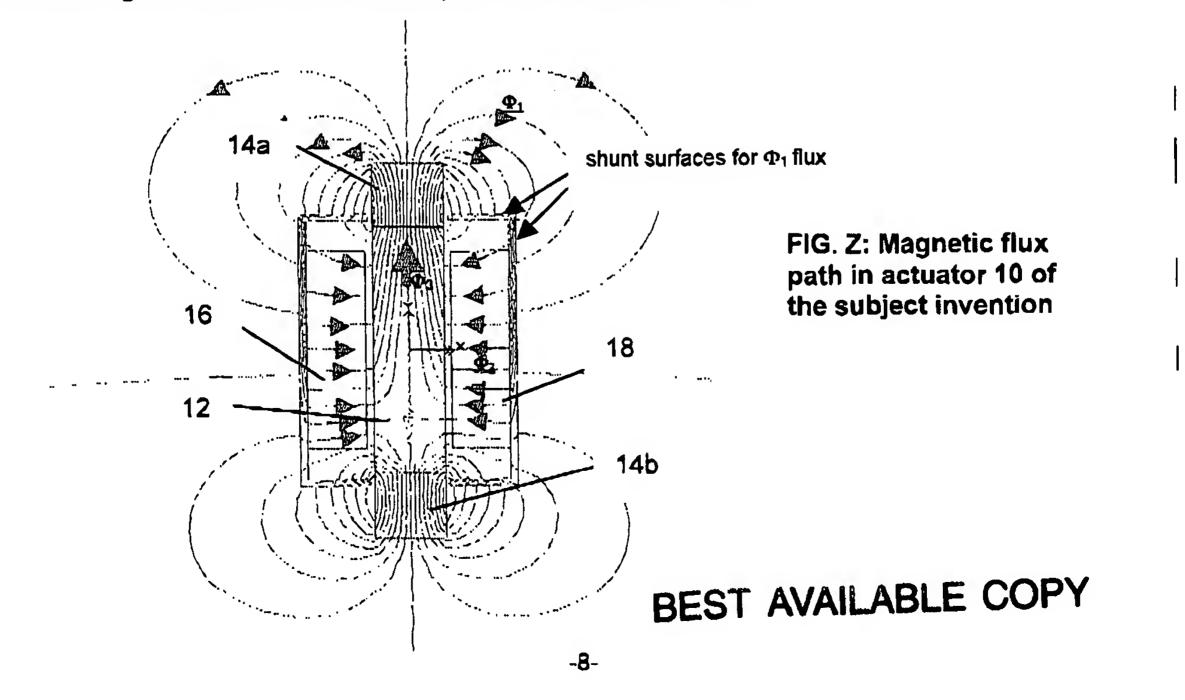
For discussion purposes, the shunt regions of yoke (44) will be hypothetically removed as shown in FIG. X above. In FIG. Y above, the yoke (44) is shown having shunt regions as disclosed throughout the Fisher reference. As shown in FIG. X, the air-gap flux  $\Phi_3$  (which generates the active force) is reduced by the leakage flux  $\Phi_1$  that crosses the solinoid (43). The flux  $\Phi_1$  creates a Lorentz force opposed by the Lorentz force created by the flux  $\Phi_2$  ( $\Phi_2$  is opposed in sign to  $\Phi_1$ ). The total active force is primarily created by the flux  $\Phi_3$  (as diminished by the flux  $\Phi_1$ ). FIG. Y shows how the Fisher

Appl. No. 10/656,257 Amendment Dated October 12, 2004 Response to Office Action of April 13, 2004

actuator (along with other conventional electromagnetic actuators) uses the shunt regions on yoke (44) to eliminate the unwanted effects of  $\Phi_1$  and  $\Phi_2$ .

In contrast, the open shield structure as defined by claim 1 of the present invention, as amended, allows the radial magnetic field generated by the permanent magnets to flow from the armature assembly through the coil (16) to the shield (18). This results in a radial magnetic field flowing from the armature assembly to the shield that generates Lorentz force. Since the shield (18) of the present invention provides a single and uninterrupted internal region that extends between the inside surfaces of the hollow tubular portion, the radial magnetic field flows from the armature assembly through the coil (16) and to the outer wall of the shield (18) (Disclosure, page 12, lines 8 to 25).

As shown in FIG. Z below, the actuator (10) of the subject invention is bi-stable and during operation, both armature magnets are always positioned substantially outside of the shield (18). Flux components  $\Phi_1$  in the subject actuator (10) (similar to  $\Phi_1$  shown in the annotated X version of Fisher FIG. 4) are shunted by the end-caps (19) while components  $\Phi_2$  (similar to  $\Phi_2$  shown in the annotated X version of Fisher FIG. 4) produce useful Lorentz force that is added to the other magnetic forces shown increasing the active force developed by the actuator (10).



Appl. No. 10/656,257

'Amendment Dated October 12, 2004

Response to Office Action of April 13, 2004

Accordingly, the actuator (10) benefits from the flux components  $\Phi_2$  that are allowed to

flow within the ferromagnetic shield (18) of the present invention since the shield (18)

has a single and uninterrupted internal surface that extends between the inside surfaces

of the hollow tubular portion.

It is submitted that the actuator disclosed in Fisher does not disclose the use of a shield

(yoke) that defines a single and uninterrupted internal region extending between the

inside surfaces of the hollow tubular portion. Rather, the yoke (44) includes shunt

regions (as circled in Fisher FIGS. 4 and 6 above) in order to shunt the radial magnetic

field that would otherwise flow from the armature assembly to the yoke (44).

Further, the specific design of the shield (18) of the present invention allows for the

generation of enough force for the entire stroke of the actuator (i.e. complete latching)

without any need for a permanent magnetic ring or other auxiliary spring elements that

prior art designs (including Fisher) use. Specifically, the  $\Phi_1$  type flux that is shunted by

the end-caps (19) and the shield (18) of the present invention, generates magnetic

latching in both stroke end positions. In Fisher, unwanted flux  $\Phi_1$  adds to the energy

losses while in the case of the present actuator (10), the flux  $\Phi_1$ , is utilized to generate

latching action. The result is that the actuator of the present invention is much smaller

and more efficient that the Fisher actuator. In space applications, additional elements

(e.g. magnetic rings) render such actuators unusable due to larger volume and mass.

Accordingly, the Applicant respectfully submits that the subject matter claimed in

independent claim 1, as amended, is not shown nor suggested by the Fisher reference.

It is further submitted that dependent claims 2 to 7, recite additional patentable features

that are neither taught nor suggested by the Fisher reference. Withdrawal of the

Examiner's rejection in respect of claims 1 to 7 is respectfully requested.

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-9-

Appl. No. 10/656,257

Amendment Dated October 12, 2004

Response to Office Action of April 13, 2004

Claim 6 rejected under 35 U.S.C. §103(a) in view of Fisher

The Examiner has rejected claim 6 under 35 U.S.C. §103(a) as being anticipated by

Fisher (U.S. Patent No. 6,040,752).

Specifically, the Examiner states that it would have been obvious to one skilled in the art

at the time the invention was made to use a bifilar wire in order to create a coil that can

be energized in the clockwise and counter-clockwise orientation using the same control

pulse on either of the two wire strands.

The Applicant submits that for the reasons discussed above in respect of claim 1, as

amended, that the subject matter claimed in dependent claim 6, as amended, is not

shown nor suggested by the Fisher reference. Withdrawal of the Examiner's rejection in

respect of claim 6 is respectfully requested.

References Made of Record and Not Relied Upon

The Applicant has briefly reviewed the other references cited by the Examiner. The

Applicant respectfully submits that these references do not recognize the problem

solved by the present invention and do not describe or even suggest the present

invention. The Applicant respectfully submits that they are not relevant to the

patentability of the claims of the present invention.

In view of the foregoing, the Applicant respectfully submits that the application is now in

condition for allowance. If the Examiner believes that a telephone interview would

expedite allowance of the application, the Examiner is respectfully requested to contact

the undersigned at (416) 364-7311.

Respectfully submitted VLADIMIRESQUET AL.

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-10-

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